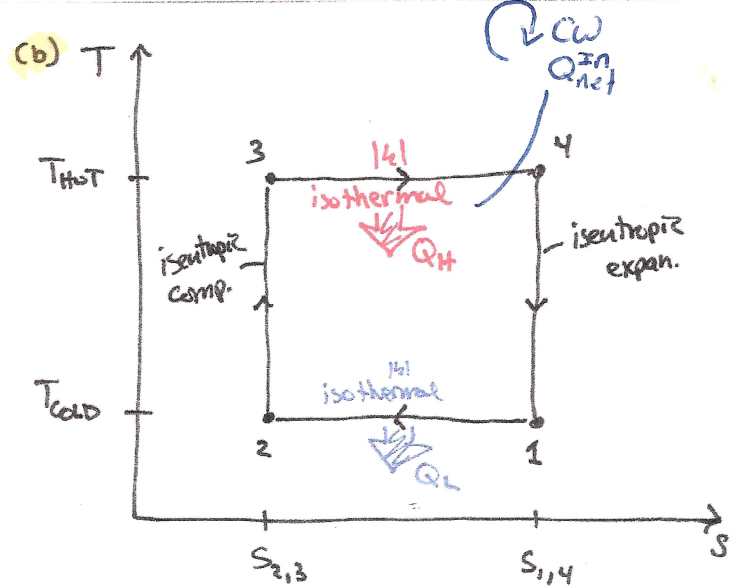
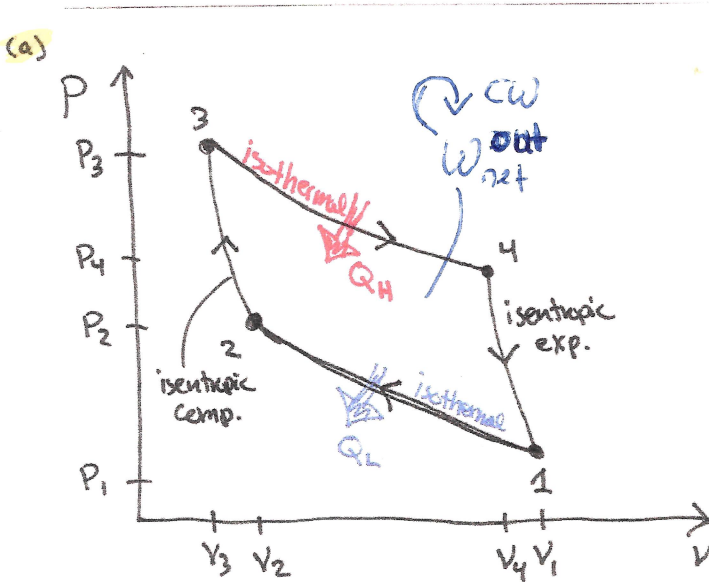


**Carnot Cycle:** The Carnot cycle is the most efficient power producing cycle that can be executed between a heat source at  $T_{HOT}$  and heat sink at  $T_{COLD}$ . The cycle is said to be reversible and can be described by the four-step cycle (process):

- 1→2: Isothermal Compression with heat rejection ( $Q_L$ ) at  $T_{COLD}$ ,
- 2→3: Isentropic Compression to the temperature of the heat source ( $T_{HOT}$ ),
- 3→4: Isothermal Expansion with heat addition ( $Q_H$ ) at  $T_{HOT}$ ,
- 4→1: Isentropic Expansion to the temperature of the heat sink ( $T_{COLD}$ ).

- (a) Sketch the  $P$  vs.  $v$  diagram for the Carnot cycle (label all key parameters and processes). [7 pts]
- (b) Sketch the  $T$  vs.  $s$  diagram for the Carnot cycle (label all key parameters and processes). [7 pts]
- (c) Derive the thermal efficiency of the Carnot cycle in terms of  $T_{COLD}$  and  $T_{HOT}$ ? [11 pts]



(c)

$$\eta_{th} = \frac{W_{net}^{out}}{Q_H} = 1 - \frac{Q_L}{Q_H}$$

$[Q_L, Q_H]$  ← derive by / with 1<sup>st</sup> and/or 2<sup>nd</sup> laws.

use 2<sup>nd</sup> law →  $Tds = Q$  (Tds equation)

$$\begin{cases} -Q_L = T_{COLD} (s_2 - s_1) \\ \Rightarrow Q_L = T_{COLD} (s_1 - s_2) \checkmark \\ +Q_H = T_{HOT} (s_4 - s_3) \checkmark \end{cases}$$

isentropic processes ...

$$s_1 = s_4, s_2 = s_3$$

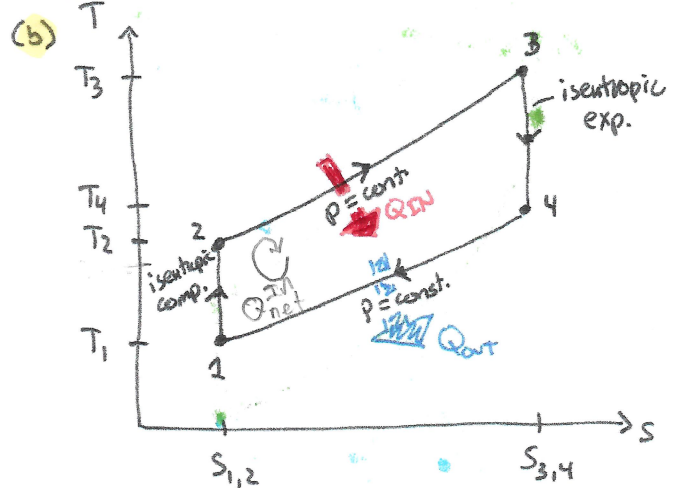
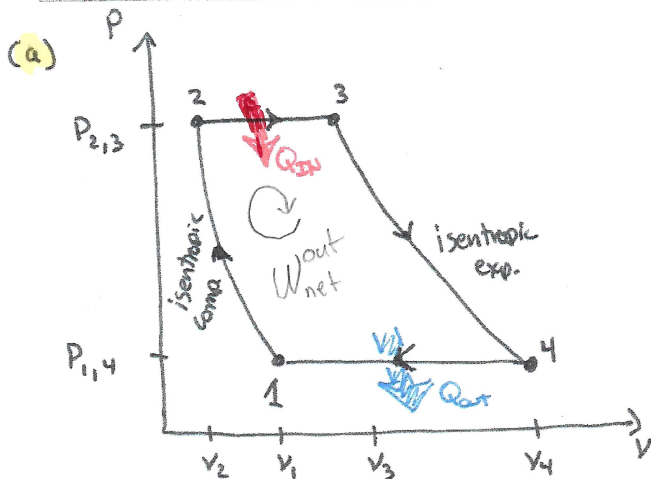
$$\eta_{th} = 1 - \frac{T_{COLD} (s_1 - s_2)}{T_{HOT} (s_4 - s_3)} = 1 - \frac{T_{COLD} (s_4 - s_3)}{T_{HOT} (s_4 - s_3)}$$

$$\Rightarrow \eta_{th} = 1 - \frac{T_{COLD}}{T_{HOT}}$$

**Ideal Brayton Cycle:** The ideal Brayton cycle represents an ideal, closed cycle for a Gas-Turbine engine. The ideal Brayton cycle is described by the four-step cycle (process):

- 1→2: Isentropic Compression (in a **compressor**),
- 2→3: Constant-pressure heat addition ( $Q_{in}$ ) to  $v_3$ ,
- 3→4: Isentropic Expansion from  $v_3$  to  $v_4$  (in a **turbine**),  $W_{in}$  for compressor?
- 4→1: Constant-pressure compression with heat rejection ( $Q_{out}$ ) back to  $v_1$ .

- (a) Sketch the  $P$  vs.  $v$  diagram for this Brayton cycle (label all key parameters and processes). [7 pts]
- (b) Sketch the  $T$  vs.  $s$  diagram for this Brayton cycle (label all key parameters and processes). [7 pts]
- (c) Derive the thermal efficiency of the ideal Brayton cycle in terms of  $T_1, T_2, T_3,$  and  $T_4$ ? [11 pts]



(c)  $\eta_{th} = \frac{W_{net}^{out}}{Q_H} = 1 - \frac{Q_{out}}{Q_{in}}$

~~$[Q_{out}, Q_{in}]$~~  ← via 1st or 2nd laws

$Q_{out}$ : 1st law  $4 \rightarrow 1$

$$(E_{mass}^{in} + Q_{in} + W_{in})_{4 \rightarrow 1} - (E_{mass}^{out} + Q_{out} + W_{out})_{4 \rightarrow 1} = \Delta U|_{4 \rightarrow 1}$$

$$\Rightarrow W_{in}|_{4 \rightarrow 1} - Q_{out} = u_1 - u_4 \Rightarrow -Q_{out} = u_1 - u_4 - W_{in}|_{4 \rightarrow 1}$$

NOTE:  $W_{in} = - \int P dv \Rightarrow W_{in}|_{4 \rightarrow 1} = P_1(v_4 - v_1)$

$$\Rightarrow Q_{out} = -(u_1 - u_4) + W_{in}|_{4 \rightarrow 1}$$

$$Q_{out} = (u_4 - u_1) + W_{in}|_{4 \rightarrow 1}$$

Prod. Rate

$$Q_{out} = (u_4 - u_1) + P_1(v_4 - v_1)$$

$$\Delta H = \Delta u + \Delta(Pv) = \Delta u + P\Delta v + v\Delta P$$

$$\Rightarrow Q_{out} = \Delta H|_{2 \rightarrow 4} \Rightarrow Q_{out} = m c_p (T_4 - T_1)$$

$Q_{in}$ : 1st law  $2 \rightarrow 3$

$$Q_{in} - W_{out} = \Delta U|_{2 \rightarrow 3}$$

$$\Rightarrow Q_{in} = \Delta U|_{2 \rightarrow 3} + W_{out}|_{2 \rightarrow 3}$$

$$= \Delta H|_{2 \rightarrow 3} \Rightarrow Q_{in} = m c_p (T_3 - T_2)$$

$$\Rightarrow \eta_{th} = 1 - \frac{m c_p (T_4 - T_1)}{m c_p (T_3 - T_2)}$$

ideal Brayton

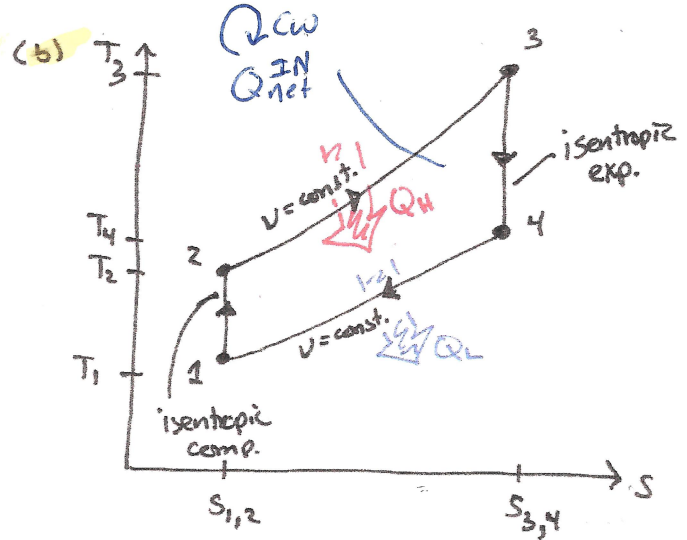
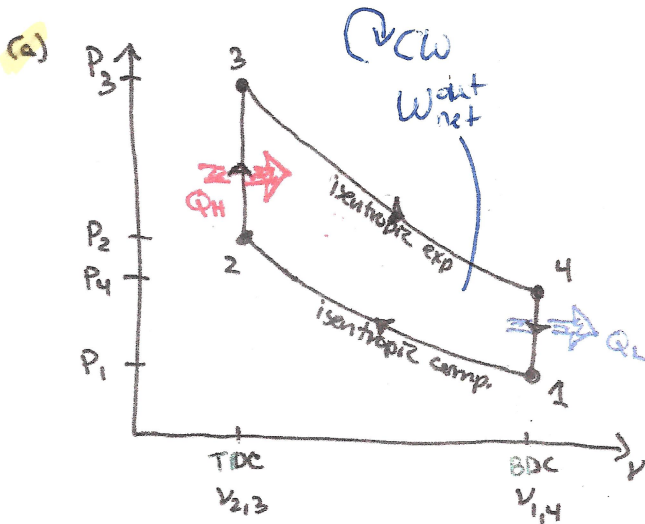
$$\eta_{th} = 1 - \frac{(T_4 - T_1)}{(T_3 - T_2)}$$

# Isentropic - $\Delta S = 0$ , undefined line

**Otto Cycle:** The Otto cycle represents the ideal cycle for Spark-Ignition engines. The ideal Otto cycle is described by the four-step cycle (process):

- 1→2: Isentropic Compression from Bottom-Dead-Center (BDC) to Top-Dead-Center (TDC),
- 2→3: Constant volume heat addition ( $Q_H$ ),
- 3→4: Isentropic Expansion from TDC ( $V_{min}$ ) to BDC ( $V_{max}$ ),
- 4→1: Constant volume heat rejection ( $Q_L$ ).

- (a) Sketch the  $P$  vs.  $v$  diagram for the Otto cycle (label all key parameters and processes). [7 pts]
- (b) Sketch the  $T$  vs.  $s$  diagram for the Otto cycle (label all key parameters and processes). [7 pts]
- (c) Derive the thermal efficiency of the Otto cycle in terms of  $T_1, T_2, T_3$ , and  $T_4$ ? [11 pts]



(c)  $\eta_{th}^{otto} = \frac{W_{net}^{out}}{Q_H} = 1 - \frac{Q_L}{Q_H}$

$[Q_L, Q_H] \leftarrow$  derive via 1st or 2nd laws

via 1st law

$Q_L:$   $E_{in} - E_{out} = \Delta U$  (for process 4→1)

note:  $W_{in} = \int_{v_4}^{v_1} P dv = 0$

$\frac{du}{dT}|_v = c_v$

$\Rightarrow (E_{mass, in} + Q_{in} + W_{in}) - (E_{mass, out} + Q_{out} + W_{out}) = \Delta U$   
 $\Rightarrow -Q_{out} = u_1 - u_4$   
 $\Rightarrow Q_L = m c_v (T_4 - T_1)$  ✓

via 1st law

$Q_H:$   $E_{in} - E_{out} = \Delta U$  (for process 2→3)

note: 2→3 (constant volume)

$\Rightarrow W_{in} = W_{out} = 0$

$\Rightarrow [E_{mass, in} + Q_{in} + W_{in}] - [E_{mass, out} + Q_{out} + W_{out}] = \Delta U$   
 $\Rightarrow Q_H = u_3 - u_2$   
 $\Rightarrow Q_H = m c_v (T_3 - T_2)$  ✓

$Q_{in} = Q_H$   
 $\frac{du}{dT}|_v = c_v$

$\Rightarrow \eta_{th}^{otto} = 1 - \frac{m c_v (T_4 - T_1)}{m c_v (T_3 - T_2)}$

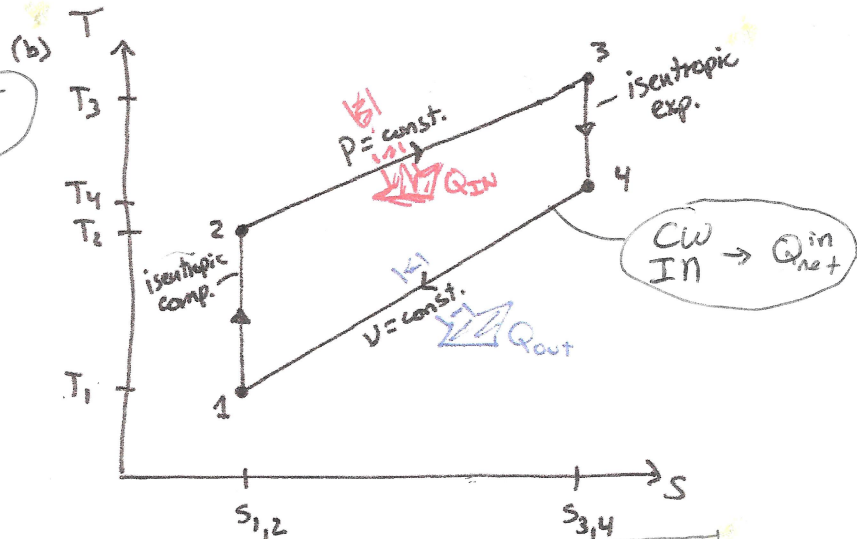
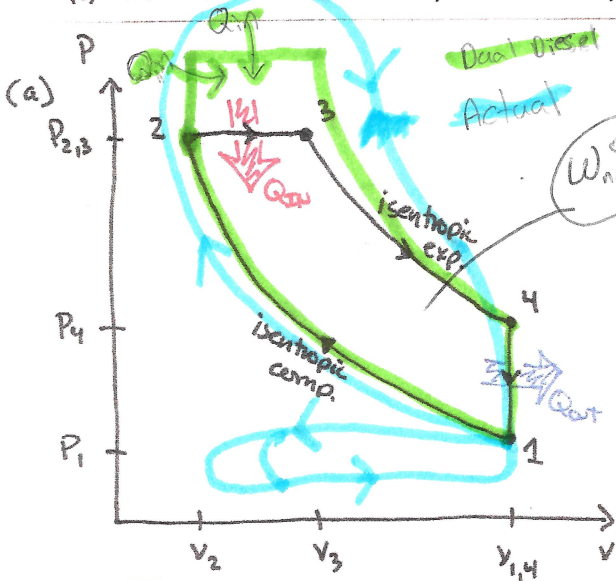
$\Rightarrow \eta_{th}^{otto} = 1 - \frac{(T_4 - T_1)}{(T_3 - T_2)}$

**Diesel Cycle:** The Diesel cycle represents the ideal cycle for Compression-Ignition engines. The ideal Diesel cycle is described by the four-step cycle (process):

- 1→2: Isentropic Compression from Bottom-Dead-Center (BDC) to Top-Dead-Center (TDC),
- 2→3: Constant pressure heat addition ( $Q_{in}$ ) to  $v_3$ ,
- 3→4: Isentropic Expansion from  $v_3$  to  $v_4$ ,
- 4→1: Constant volume heat rejection ( $Q_{out}$ ) at TDC ( $v_1$ ).

$\Delta S = 0$  for isentropic  
 $T \uparrow$  for isentropic comp

- (a) Sketch the  $P$  vs.  $v$  diagram for the Diesel cycle (label all key parameters and processes). [7 pts]
- (b) Sketch the  $T$  vs.  $s$  diagram for the Diesel cycle (label all key parameters and processes). [7 pts]
- (c) Derive the thermal efficiency of the Diesel cycle in terms of  $k$ ,  $T_1$ ,  $T_2$ ,  $T_3$ , and  $T_4$ ? [11 pts]



(c)  $\eta_{th} = \frac{W_{net}^{out}}{Q_H} = 1 - \frac{Q_L}{Q_H}$  [ $Q_L, Q_H$ ] ← via 1st or 2nd law

$k = \frac{c_p}{c_v}$

$Q_L$ : (1st law)  $\xrightarrow{4 \rightarrow 1} (E_{mass}^{in} + Q_{in} + W_{in}) - (E_{mass}^{out} + Q_{out} + W_{out}) = \Delta U|_{4 \rightarrow 1}$   
 $\Rightarrow -Q_{out} = u_1 - u_4, Q_{out} = Q_L, \frac{du}{dT}|_v = c_v \Rightarrow -Q_L = mc_v(T_1 - T_4)$

$Q_L = mc_v(T_4 - T_1)$

$Q_H$ : (1st law)  $\xrightarrow{2 \rightarrow 3} (E_{mass}^{in} + Q_{in} + W_{in}) - (E_{mass}^{out} + Q_{out} + W_{out}) = \Delta U|_{2 \rightarrow 3}$

$Q_{in} = Q_H \Rightarrow Q_H - W_{out} = u_3 - u_2 \Rightarrow Q_H = \Delta U|_{2 \rightarrow 3} + W_{out}|_{2 \rightarrow 3}$

NOTE:  $\Delta H|_{2 \rightarrow 3} = \Delta U|_{2 \rightarrow 3} + \Delta(PV)|_{2 \rightarrow 3} = (u_3 - u_2) + P\Delta V|_{2 \rightarrow 3} + V(\Delta P)|_{2 \rightarrow 3}$

$W_{out}|_{2 \rightarrow 3} = \int_{v_2}^{v_3} P dv = P_2(v_3 - v_2)$

$\Rightarrow Q_H = \Delta H|_{2 \rightarrow 3} \Rightarrow Q_H = mc_p(T_3 - T_2)$

$\Rightarrow \eta_{th} = 1 - \frac{mc_v(T_4 - T_1)}{mc_p(T_3 - T_2)} = 1 - \frac{c_v(T_4 - T_1)}{c_p(T_3 - T_2)}$

$k = \frac{c_p}{c_v} \Rightarrow \eta_{th} = 1 - \frac{(T_4 - T_1)}{k(T_3 - T_2)}$